

**FLOW AND HEAT TRANSFER IN A POROUS MEDIUM DUE TO AN
OSCILLATING PLATE WITH OSCILLATING TEMPERATURE IN A
VISCOUS FLUID NEAR ITS SURFACE**

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Abstract

The induced flow and the heat transfer in a porous medium have been discussed when a flat plate parallel to the porous surface oscillates in its own plane with its temperature also oscillating. The gap between two surfaces is filled with a viscous fluid which also fully saturates the porous medium. It is found that when the porous medium is unbounded the amplitude of oscillation of the fluid at the interface increases with the increase of the permeability of the porous medium and also with the increase of Reynolds number. There is a boundary layer formation at the interface in the porous region when the thicknesses of the porous material and the clear fluid are equal. The case when thickness of the porous layer is one-tenth of that of the clear fluid, this system produces a cooling, effect on the porous surface.

Mathematics Subject Classification (2000) 76S05.

Key words: Flow, Heat transfer, porous medium, Oscillating Plate and temperature.

1. Introduction

The flow of a viscous fluid and the heat transfer through a porous medium have broad range application in geothermal system, thermal installation, metal processing, catalytic reaction, filtration and transpiration cooling. Vafai and Tien [1], Vafai [2] and Beckerman and Viskanta [3] have studied the effect of

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1. Introduction

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variable porosity and variation in the boundary layer and temperature in forced convection boundary layer flow, heat and mass transfer along a flat plate embedded in a porous medium.

The object of this paper is to study the induced flow and the effect of cooling in a porous medium when an infinite flat plate parallel to the porous surface oscillates in its own plane. The space between the plate and the porous medium is filled with an incompressible viscous fluid with which the porous medium is fully saturated. The temperature of the oscillating plate also oscillates with the same frequency as that of the oscillation of the plate. It is assumed that Navier-Stokes equation and Brinkman equation [4] respectively govern the flow in the clear fluid region, called region I and in the porous region, called region II. At the interface of these two regions the conditions on velocity and stresses suggested by Ochoa-Tapia and Whitaker [6] are taken and we have proposed that similar conditions on the temperature be taken at the interface. Our results show that the induced steady temperature is such that cooling effects are produced in the porous medium.

Cooling problem has assumed a continuously growing importance in the development of high speed vehicles (like space vehicles, aircrafts, missiles etc.) One of the effective method of cooling is the transpiration cooling in which the surfaces to be protected are manufactured from porous materials and cold fluid is ejected from the pores (See Shivakumara and Venkatachalappa [6]). Another method is that the surface to be protected from hot fluid is lined with porous material and our results are useful in this case.

2. Statement of the problem :

Consider the flow and the heat transfer of an incompressible viscous fluid confined between an infinite impervious flat plate executing linear harmonic oscillation of frequency n parallel to itself and a porous medium fully saturated with the fluid. Temperature of the oscillating plate also oscillates with frequency n . Let x denote the coordinate parallel to the direction of motion and y the

coordinate perpendicular to the plate. Let the oscillating plate be represented by $y = d$, the interface by $y = 0$ and the plane bounding the porous medium by $y = -\lambda d$ where λ is a real constant. The schematic of the problem is given in figure 1. In the region I the flow is governed by Navier-Stokes equation and in region II it is governed by Brinkman equation [4]. The only velocity component in the direction of x and the temperature are functions of y and t only and are respectively denoted by $u(y,t)$, $T(y,t)$ in the region I and $U(y,t)$, $H(y,t)$ in the region II. The boundary conditions of the problem are :

$$u = U_0 \cos(nt) \text{ at } y = d, \quad (1)$$

$$T = T_w + T_0 \cos(nt) \text{ at } y = d, \quad (2)$$

$$U = 0 \text{ at } y = -\lambda d, \quad (3)$$

$$H = T_w \text{ at } y = -\lambda d. \quad (4)$$

At the interface of the porous medium and clear fluid $y = 0$, we assume that the velocity component is continuous and the jump in the shearing stress T_{yx} is given by the equation suggested by Ochoa-Tapia and Whitaker [5]. These assumptions in our notation can be written as :

$$u = U \text{ at } y = 0, \quad (5)$$

$$\mu \frac{\partial U}{\partial y} - \mu \frac{\partial u}{\partial y} = \frac{\beta \mu}{\sqrt{k}} U \text{ at } y = 0 \quad (6)$$

where μ is the viscosity of the fluid, k is the permeability of the porous medium and β is a constant which takes positive as well as negative values and depends on the nature of the porous surface (See Ochoa-Tapia and Whitaker [7]). Using these conditions at the interface Srivastava [8] has discussed the torsional oscillation of an infinite disk in a viscous liquid bounded by a porous medium. On the similar basis we propose that temperature is continuous at the interface and there is a jump in the heat flux at the interface which is proportional to the temperature at the interface. This can be written as :

$$T = H \text{ at } y = 0, \quad (7)$$

$$K \frac{\partial H}{\partial y} - K \frac{\partial T}{\partial y} = \frac{\alpha K}{\sqrt{k}} T \quad \text{at } y = 0, \quad (8)$$

where K is the thermal conductivity and α is a constant depending on the surface of the porous medium and its value is similar to that of β .

The equations governing the velocity and temperature in regional I respectively given by

$$\frac{\partial u}{\partial t} = \nu \frac{\partial^2 u}{\partial y^2}, \quad (9)$$

$$\rho g C_p \frac{\partial T}{\partial t} = K \frac{\partial^2 T}{\partial y^2} + \mu \left(\frac{\partial u}{\partial y} \right)^2, \quad (10)$$

where ν is the kinematic coefficient of viscosity, p is the density, g is the acceleration due to gravity and C_p is the specific heat at constant pressure. The equations governing the velocity and temperature in region II, are respectively given by

$$\frac{\partial U}{\partial t} = \nu \frac{\partial^2 U}{\partial y^2} - \frac{\nu}{k} U, \quad (11)$$

$$\rho g C_p \frac{\partial H}{\partial t} = K \frac{\partial^2 H}{\partial y^2} + \mu \left(\frac{\partial U}{\partial y} \right)^2 + \frac{\mu}{k} U^2 \quad (12)$$

The equation (12) is written by taking dissipation due to viscosity as well as due to permeability. Srivastava and Sharma [9] have studied the heat transfer in a porous medium due to rotation of a disk near its surface by taking equation (12) for temperature distribution.

3. The Velocity Field :

We adopt here the complex notation with the convention that only the real parts of the complex quantities represent the physical quantities. Under this notation boundary condition (1) is written as :

$$u = U_0 e^{i\tau} \quad \text{at } y = d, \quad (13)$$

where $\tau = nt$. We assume the following expressions for the velocity in region I and II respectively

$$u = U_0 g(\eta)e^{i\tau}, \quad (14)$$

$$u = U_0 G(\eta)e^{i\tau}, \quad (15)$$

where $\eta = (y/d)$. The equations (9) and (11) give the following equations for $g(\eta)$ and $G(\eta)$ respectively :

$$i \operatorname{Re} g = g'', \quad (16)$$

$$(i \operatorname{Re} + \sigma^2)G = G'', \quad (17)$$

where $\sigma = (d/\sqrt{k})$, Reynold's number $\operatorname{Re} = (nd^2/\nu)$ and a prime denotes differentiation with respect to η .

The boundary conditions (1) and (3) give

$$g(1) = 1, \quad (18)$$

$$G(-\lambda) = 0, \quad (19)$$

The matching conditions at the interface (5) and (6) become

$$g(0) = G(0), \quad (20)$$

$$G'(0) - g'(0) = \beta\sigma G(0) \quad (21)$$

The solutions of the equations (16) and (17) satisfying (18) - (21) are

$$g(\eta) = (1/\operatorname{sh} p) [C_1 \operatorname{sh} \lambda q \operatorname{sh} p(1-\eta) + \operatorname{sh} p\eta], \quad (22)$$

$$G(\eta) = C_1 \operatorname{sh} q(\lambda+\eta), \quad (23)$$

where $(1/C_1) = (1/p) [p \operatorname{sh} \lambda q \operatorname{ch} p + q \operatorname{sh} p \operatorname{ch} \lambda q - \beta\sigma \operatorname{sh} \lambda q \operatorname{sh} p] = A_1 e^{i\theta_1}$ (24)

$$p = (1+i)\sqrt{(\operatorname{Re}/2)}, \quad q = a_1 + ia_2 = a \left[\operatorname{Cos}\left(\frac{\theta}{2}\right) + i \operatorname{Sin}\left(\frac{\theta}{2}\right) \right]$$

$$a = (\operatorname{Re}^2 + \sigma^4)^{\frac{1}{4}}, \quad \tan \theta = (\operatorname{Re}/\sigma^2)$$

In writing the above solution $\cosh \chi$ and $\sinh \chi$ are written as $\text{ch } \chi$ and $\text{sh } \chi$ respectively.

The case when the porous region is unbounded can be deduced from the above solution by taking limits of the expressions as $\lambda \rightarrow \infty$.

The expression for $g(\eta)$ is unchanged except that the value of C_1 is modified as

$$\lim_{\lambda \rightarrow \infty} C_1 = (i/p) \left[p \text{ ch } p + (q - \beta\sigma) \text{sh } p \right] = A_2 e^{i\phi_2} \quad (25)$$

The expression for $G(\eta)$ is given by

$$G(\eta) = (1/A_2) e^{q\eta - i\phi_2} \quad (26)$$

The case when $\lambda = 1$, the amplitude of oscillation of the induced velocity in the porous region is given by

$$|U| = (U_0/A_3) \left[\text{ch } 2a_1(1+\eta) - \text{Cos } 2a_2(1+\eta) \right]^{\frac{1}{2}} \quad (27)$$

where

$$(1/p)(p \text{ sh } q \text{ ch } p + q \text{ sh } p \text{ ch } q - \beta\sigma \text{ sh } p \text{ sh } q) = A_3 e^{i\phi_3} \quad (28)$$

4. Temperature Field :

The viscous dissipation function in equation (10) can be written as :

$$\begin{aligned} \left(\frac{\partial u}{\partial y} \right)^2 &= U_0^2 \left[\text{Real} \left(\frac{\partial g}{\partial y} e^{i\tau} \right) \right]^2 \\ &= \frac{U_0^2}{2} \frac{\partial g}{\partial y} \cdot \frac{\partial \bar{g}}{\partial y} + U_0^2 \text{Re al} \left[\frac{1}{2} \left(\frac{\partial g}{\partial y} \right)^2 e^{2i\tau} \right] \end{aligned} \quad (29)$$

where \bar{g} is the conjugate complex of g . Similar expressions can be written for U^2

and $\left(\frac{\partial U}{\partial y} \right)^2$ in the equation (12). Hence, the temperature field consists of three

parts the first part and the second part oscillate with frequencies n and $2n$ respectively and the third part is steady one independent of time. We assume the following form of the temperature in the region I and region II respectively

$$T - T_w = T_0[h_1(\eta) e^{i\tau} + h_2(\eta) e^{2i\tau} + h_3(\eta)], \quad (30)$$

$$H - T_w = T_0[H_1(\eta) e^{i\tau} + M_2(\eta) e^{2i\tau} + M_3(\eta)], \quad (31)$$

The boundary conditions (2) and (4) give respectively the following conditions:

$$h_i(1) = 1, \quad h_i(1) = 0, \quad i = 2, 3 \quad (32)$$

$$H_i(-\lambda) = 0, \quad i = 1, 2, 3, \quad (33)$$

Matching conditions (7) and (8) at the interface in terms of h_i and H_i can be written as :

$$h_i(0) = H_i(0), \quad i = 1, 2, 3 \quad (34)$$

$$\frac{dH_i}{d\eta} - \frac{\partial h_i}{\partial \eta} = a \sigma H_i, \quad i = 1, 2, 3 \quad (35)$$

Substituting (30) and (31) in (10) and (12) respectively and equating coefficient of $e^{i\tau}$, $e^{2i\tau}$ and terms independent of time on both sides of the equations we get the following differential equations for $h_1(\eta)$, $H_1(\eta)$, $h_2(\eta)$, $H_2(\eta)$, $h_3(\eta)$, $H_3(\eta)$:

$$i \operatorname{Re} P_r \quad h_1 = \frac{d^2 h_1}{d\eta^2}, \quad (36)$$

$$i \operatorname{Re} P_r \quad H_1 = \frac{d^2 H_1}{d\eta^2} \quad (37)$$

$$2 i \operatorname{Re} P_r \quad h_2 = \frac{d^2 h_2}{d\eta^2} + \left(\frac{EP_r}{2}\right) \left(\frac{dg}{d\eta}\right)^2, \quad (38)$$

$$2 i \operatorname{Re} P_r \quad H_2 = \frac{d^2 H_2}{d\eta^2} + \left(\frac{EP_r}{2}\right) \left[\left(\frac{dG}{d\eta}\right)^2 + \sigma^2 G^2\right], \quad (39)$$

$$\frac{d^2 h_3}{d\eta^2} = -\left(\frac{EP_r}{2}\right) \left|\frac{dg}{d\eta}\right|^2, \quad (40)$$

$$\frac{d^2 H_3}{d\eta^2} = -\left(\frac{EP_r}{2}\right) \left[\left| \frac{dG}{d\eta} \right|^2 + \sigma^2 |G|^2 \right], \quad (4)$$

where $Pr = (\mu g C_p / K)$ is the Prandtl number and $E = \left[U_0^2 / (g C_p T_0) \right]$ is Eckert number.

The solutions of (36) and (37) satisfying (32) - (35) are :

$$h_1(\eta) = (1/sh m) [C_4 sh \lambda m sh (1-\eta)m + sh m \eta] \quad (4)$$

$$H_1(\eta) = C_4 sh m (\lambda + \eta), \quad (4)$$

$$(1/C_4) = (1/m) [m sh \lambda m ch m + m sh m ch \lambda m - \alpha \sigma sh \lambda m sh m]$$

where $m = (1+i)\sqrt{(\text{Re } P_r/2)}$. This is the case of pure conduction as there is no term involving convection in the differential equations. Substituting expressions of $g(\eta)$ and $G(\eta)$ from (22) and (23) in the equations (38) and (39) respectively, we get the following solutions for $h_2(\eta)$ and $H_2(\eta)$:

$$h_2(\eta) = \frac{EP_r p^2}{8sh^2 p} \left[-B_1 ch m \eta \sqrt{2} + B_2 sh m \eta \sqrt{2} - \frac{ch 2p\eta + C_1^2 sh^2 \lambda q ch 2p(1-\eta) - 2C_1 sh \lambda q ch p(1-2\eta)}{2p^2 - i \text{Re } P_r} + \frac{i(1 + C_1^2 sh^2 \lambda q - 2C_1 sh \lambda q ch p)}{\text{Re } P_r} \right],$$

$$H_2(\eta) = \frac{EP_r C_1^2}{8} \left[D_1 ch m \eta \sqrt{2} + D_2 sh m \eta \sqrt{2} - \frac{(q^2 + \sigma^2) ch 2q(\lambda + \eta)}{2q^2 - i \text{Re } P_r} + \frac{i(q^2 - \sigma^2)}{\text{Re } P_r} \right],$$

Constants B_1, B_2, D_1, D_2 can be determined by substituting (44) and (45) in (32) - (35). For the present we are interested in steady part only so we have not determined them.

Substituting the expressions of $g(\eta)$ and $G(\eta)$ from (22) and (23) in the equation (40) and (41) we get the following solutions for $h_3(\eta)$ and $H_3(\eta)$

$$\begin{aligned}
 h_3(\eta) = & \frac{EP_r}{8(ch2\sqrt{Re} - Cos2\sqrt{Re})} \left[\left(\frac{b}{A_1} \right)^2 \left\{ Cos2(1-\eta)\sqrt{Re} \right. \right. \\
 & \left. \left. - ch2(1-\eta)\sqrt{Re} \right\} + \left(\frac{2b}{A_1} \right) \left\{ Cos(1-2\eta)\sqrt{Re}ch\sqrt{Re} - ch(1-2\eta)\sqrt{Re}Cos\sqrt{Re} \right\} \right. \\
 & \left. Cos(\psi - \phi_1) + (Cos2\eta\sqrt{Re} - Cos2\sqrt{Re}) - (ch2\eta\sqrt{Re} - ch2\sqrt{Re}) \right] \\
 & + \left(\frac{EP_r}{16} \right) (1-\eta)M_1, \tag{46}
 \end{aligned}$$

$$\begin{aligned}
 H_3(\eta) = & \frac{EP_r}{(4A_1\lambda a_1 a_2)^2} \left[a_1^2 \left\{ \sqrt{(Re^2 + \sigma^4)} - \sigma^2 \right\} \left\{ Cos2\lambda(1+\eta)a_2 - 1 \right\} \right. \\
 & \left. - a_2^2 \left\{ \sqrt{(Re^2 + \sigma^4)} + \sigma^2 \right\} \left\{ ch2\lambda(1+\eta)a_1 - 1 \right\} \right] \\
 & + \left(\frac{EP_r}{16} \right) (\lambda + \eta)M_2 \tag{47}
 \end{aligned}$$

where $sh \lambda q = be^{i\psi}$. These expressions for $h_3(\eta)$ and $H_3(\eta)$ satisfy the boundary conditions (32) and (33). Two constants M_1 and M_2 are determined by the conditions (34) and (35) which can be written as :

$$M_1 - \lambda M_2 = \frac{1}{(\lambda a_1 a_2 A_1)^2} \left[a_1^2 \left\{ \sqrt{(Re^2 + \sigma^4)} - \sigma^2 \right\} (Cos2\lambda a_2 - 1) - a_2^2 \right]$$

$$\left\{ \sqrt{(\text{Re}^2 + \sigma^4)} + \sigma^2 \right\} (ch2\lambda a_1 - 1) \left] + 2 \left[\left(\frac{b}{A_1} \right)^2 + 1 \right] \right. \quad (48)$$

$$(1 + \alpha\sigma)M_1 + M_2 = 2\alpha\sigma \left\{ \left(\frac{b}{A_1} \right)^2 + 1 \right\} + \frac{4\sqrt{\text{Re}}}{ch2\sqrt{\text{Re}} - \text{Cos}2\sqrt{\text{Re}}} \\ \left[\left(\frac{b}{A_1} \right)^2 (\text{Sin}2\sqrt{\text{Re}} + sh2\sqrt{\text{Re}}) + \left(\frac{2b}{A_1} \right) (\text{Sin}\sqrt{\text{Re}} \ ch\sqrt{\text{Re}} \right. \\ \left. + \text{Cos}\sqrt{\text{Re}} \ sh\sqrt{\text{Re}} \right) \text{Cos}(\psi - \phi_1) \left] - \frac{2}{\lambda a_1 a_2 A_1^2} \left[a_1 \left\{ \sqrt{(\text{Re}^2 + \sigma^4)} - \sigma^2 \right\} \right. \\ \left. \text{Sin}2\lambda a_2 + a_2 \left\{ \sqrt{(\text{Re}^2 + \sigma^4)} - \sigma^2 \right\} sh2\lambda a_1 \right] \quad (49)$$

5. Discussions and Conclusions :

The induced velocity in the porous medium when it is unbounded below is given by substituting (26) in (15) as :

$$U = (U_0/A_2)e^{a_1\eta} \text{Cos}(\tau + a_2\eta - \phi_2) \quad (50)$$

This shows that the induced velocity in the porous medium has the form of damped harmonic oscillations the amplitude of which is $(U_0/A_2)e^{a_1\eta}$. The fluid layer at a distance $(2\pi d/a_2) = 2\pi[2\nu k/\{(n^2k^2 - \nu^2) - \nu\}]^{1/2}$ apart oscillates with the same phase and this distance is called the depth of penetration of the viscous layer (See Schlichting [10]).

The amplitude of oscillations of the fluid velocity at the interface is given by (U_0/A_2) . The value of $(A_2)^{-1}$ has been is table 1 for $\sigma = 5, 6, 7, 8, 9, 10$; $\text{Re} = 2, 3, 4$ and $\beta = -0, 5, 0.5$. The table 1 shows that amplitude of oscillations of the fluid decreases with the increase of σ for all values of Re and β . It increases with the increase of Re for all values of σ and β . It decreases much with the

decrease of β and its values for $\beta = -0.5$ is less than half of those for $\beta = 0.5$. The values of β for the porous surfaces depends on the porous material and can be experimentally determined from other experiments (See Ochoa - Tapia and Whitaker [7]).

In the case $\lambda = 1$, the amplitude of the fluid oscillations in the porous medium is given by

$$|(U/U_0)| = (1/A_3) \left[Ch \ 2a_1(1+\eta) - Cos \ 2a_2(1+\eta) \right]^{\frac{1}{2}} \quad (51)$$

where $A_3 = |(1/p)(p \ sh \ q \ ch \ p + q \ sh \ p \ ch - \beta \sigma \ sh \ p \ sh q)|$

Taking $Re = 2$, $\beta = 0.5$ the graph of $|(U/U_0)|$ has been drawn against η from $\eta = 0$ to -1.0 for $\sigma = 5, 6, 7, 8$. The graph shows that this amplitude reduces with the increase of σ and there is a boundary formation near the interface. Comparing the values of $|(U/U_0)|_{\eta=0}$ in the graph and those given in the table 1 we find that these reduce much when the porous medium is bounded by another plane below.

Now we will discuss the case of steady heat transfer where there is a lining of a surface by a porous material. The rate of the heat transfer at the nominal surface (interface) $\eta = 0$ from the porous material to the clear fluid is given by :

$$Q = -K \left(\frac{\partial T}{\partial Y} \right)_{y=0} = \left(\frac{KT_0}{d} \right) N \quad (53)$$

where N is the Nusselt number given by

$$N = - \left(\frac{dH_3}{d\eta} \right)_{\eta=0} \quad (54)$$

Substituting the value of $H_3(\eta)$ from (47) in (54) we get

$$N = \frac{EP_r}{8A_1^2 \lambda a_1 a_2} \left[\left\{ \sqrt{(Re^2 + \sigma^4)} + \sigma^4 \right\} a_2 \ sh \ 2\lambda a_1 \right]$$

$$+ \left\{ \sqrt{(\text{Re}^2 + \sigma^4)} - \sigma^2 \right\} a_1 \sin 2\lambda a_2 \left] - \frac{EP_r}{16} M_2 \quad (55)$$

The values of N are positive, hence heat transfer takes place from the porous surface to the clear fluid and there is cooling of the porous material. Hence when a surface is lined with a porous material surrounded by an oscillating fluid the surface is cooled. The oscillation of temperature is not important as it gives only conduction effect. Taking $\lambda = 0.1$, the ratio of N to the product of E and P_r is given in table 2 for $\alpha = 0.5, \beta = 0.5, -0.5$; $\text{Re} = 2, 3, 4$; $\sigma = 5, 6, 7, 8, 9, 10$. Table 2 shows that the rate of cooling decreases with increase of σ as well as Re for $\beta = 0.5$. For $\beta = -0.5$ this cooling rate increases with increase of Re but decreases with increase of σ . It is very much reduced with the decrease of β whose values are determined experimentally. Hence such porous lining would be done with material having high values of β .

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		$\beta = 0.5$			$\beta = -0.5$			
		Re	2	3	4	2	3	4
σ								
5			0.36901	0.43724	0.47103	0.16122	0.17884	0.20407
6			0.32906	0.38972	0.42805	0.13784	0.15797	0.17253
7			0.29456	0.34888	0.38695	0.11989	0.12906	0.14855
8			0.26868	0.31427	0.35134	0.10794	0.11312	0.13056
9			0.24681	0.28511	0.32093	0.09655	0.10065	0.11602
10			0.22641	0.26027	0.29451	0.08654	0.09062	0.10457

Table 1. : Amplitude of oscillation of the fluid at the interface.

σ	$\beta = 0.5$			$\beta = -0.5$			
	Re	2	3	4	2	3	4
5		0.86903	0.74755	0.63428	0.21356	0.23123	0.23973
6		0.76408	0.55763	0.52476	0.11360	0.12097	0.12408
7		0.53491	0.45939	0.39197	0.07896	0.08326	0.08515
8		0.47760	0.39439	0.34437	0.06103	0.06384	0.06471
9		0.42089	0.34626	0.29729	0.04996	0.05196	0.05288
10		0.37622	0.30940	0.26377	0.04238	0.04391	0.04452

Table 2. : The value of (N/EP_r) for $\alpha = 0.5$.

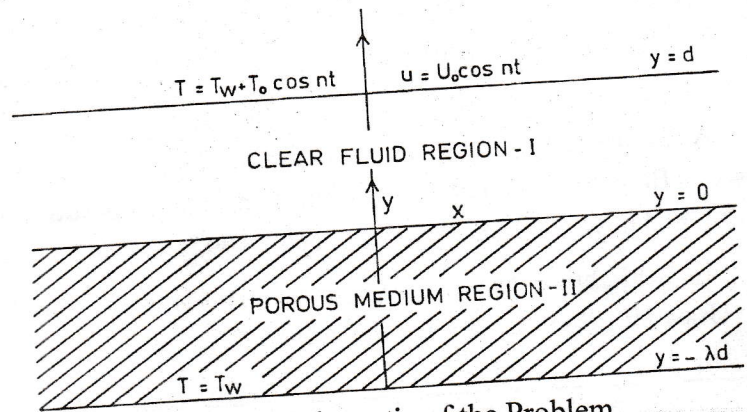


Figure 1. Schematic of the Problem.

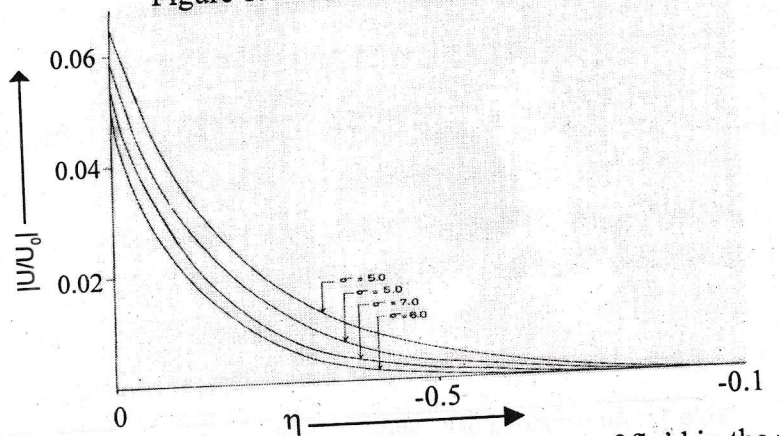


Figure 2. The graph of the amplitude of oscillations of fluid in the porous medium against the distance from interface.